# Bonding Strength of Some Adhesives in Heat-Treated Hornbeam (*Carpinus betulus* L.) Wood Used for Interior and Exterior Decoration

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Heat-treated wood has an ever-expanding market for exterior and interior applications. The objective of this study was to determine the effect of a heat treatment on the bonding strength of hornbeam (*Carpinus betulus* L.) wood that was bonded with melamine formaldehyde (MF), polyurethane (PUR), and polyvinyl acetate (PVAc-D4) adhesives. Hornbeam lamellas were heat treated at 150 °C, 175 °C, 200 °C, and 225 °C for 3 h and then bonded. The bonding strength of the specimens was determined. In addition, the density, weight loss, and pH value of the heat-treated wood were investigated. The results showed that the bonding strengths of the heat-treated wood specimens decreased with the temperature of the heat treatment. The bonding strength of the PUR adhesive was higher than the MF and the PVAc-D4.

Keywords: Heat treatment; Glue; Bonding strength; Hornbeam (Carpinus betulus L.)

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## INTRODUCTION

Heat treatment has become an increasingly important commercial application to improve the dimensional stability and bio-durability of wood (Esteves and Pereira 2009). Different thermal treatment methods significantly improve and enhance some properties of wood without the use of chemical additives (Johansson 2008). All of the processes use sawn wood and treatment temperatures between 160 °C and 260 °C. The main differences are in the process conditions (*e.g.*, the process steps, oxygen or nitrogen steaming, wet or dry process, the use of oils, and steering schedules) (Militz 2002).

During heat treatment, a large number of chemical changes occur in the wood components (Pavlo and Niemz 2003). The changes start with the deacetylation of hemicelluloses, followed by depolymerization catalyzed by the released acetic acid. Thermal modification at high temperatures leads to chemical changes of the wood constituents. First the hemicelluloses degrade, due to their low molecular weight and their branching structure, followed by the cellulose and lignin (Fengel and Wegener 1984; Tjeerdsma *et al.* 1998; Sivonen *et al.* 2002; Nuopponen *et al.* 2004).

The strong bonding strength between the wood material and adhesive depends on a number of factors, including the wettability of the wood surface, the roughness of the wood surface, the penetration behavior, the moisture content, the presence of extractives, the hygroscopicity, chemical composition, and the pH of the wood (Sahin Kol *et al.* 2009). The changes in chemical, physical, and structural properties of wood after heat treatment

can affect the overall bonding process with an adhesive (Kariz and Sernek 2010). With thermal degradation, wood loses mass to a degree that depends on the heat treatment conditions; at the same time there are significant changes in the surface properties that affect the wood bonding (Gunduz and Aydemir 2009; Kariz and Sernek 2010). Percin and Uzun (2014) examined the effects of a heat treatment on the bonding strength of Scotch pine (Pinus sylvestris L.), beech (Fagus orientalis L.), oak (Quercus petraea L.), and poplar (Populus nigra L.). The bonding strength values decreased with increasing treatment temperature. Esen and Ozcan (2012) studied the effects of heat treatment on the shear strength of oak (Quercus petraea L.) wood. For this aim, the samples were exposed to heat treatment at 170 °C, 190 °C, and 210 °C, for 2 h, 6 h, and 10 h. The samples were then bonded with phenol formaldehyde (FF), melamine formaldehyde (MF), melamine urea formaldehyde (MUF), and polyurethane (PUR) adhesives. The heat treatment decreased the shear strength values as the treatment temperature and duration increased. The most important factors affecting the shear strength of wood and wood-based material are the wood species, adhesive type, wood density, log temperature during the veneer peeling or clipping, veneer drying temperature, and the relative moisture content of wood (Demirkir et al. 2013). Yorur et al. (2014) studied the effect of humidity-water-heat tests on the bonding strength of impregnated oak (Quercus petraea spp.) bonded with UF, Desmodur-VTKA (Desmodur-Vinil trieketonol acetate), and polyvinyl acetate (PVAc) adhesives. The bonding strengths of impregnated wood samples exposed to humidresistance test samples decreased, and the bonding strength of VTKA was higher than that of the UF and PVAc adhesives.

Heat-treated wood is mainly utilized in exterior applications such as exterior cladding, window and door joinery, garden furniture, and decking. There are also many indoor applications for heat-treated wood, such as flooring, paneling, kitchen furnishing, and the interiors of bathrooms and saunas. Heat-treated wood might also have potential as a material for construction use, such as for structural elements in the building industry (Korkut 2007; Sernek *et al.* 2008).

Heat-treated wood has a growing market for exterior and interior applications, such as hornbeam (*Carpinus betulus* L.) wood used in the furniture and the woodworking industry. Therefore, knowledge of the bonding strength of heat-treated hornbeam wood may be important for exterior and interior uses. This study evaluated the bonding strength of heat-treated hornbeam wood bonded with exterior and interior structural adhesives including melamine formaldehyde, polyurethane, and polyvinyl acetate, which are used widely in the furniture and woodworking industry.

#### **EXPERIMENTAL**

#### Materials

In this study, hornbeam (*Carpinus betulus* L.) was chosen randomly from a timber supplier in Siteler, Ankara, Turkey. Hornbeam wood has widespread usage in wood working industrial in Turkey. Accordingly, non-deficient, whole, knotless, and normally grown (without zone line, reaction wood, decay, insect or fungal infection) wood materials were selected.

Wood samples with the dimensions of 10 mm  $\times$  60 mm  $\times$  550 mm were cut from the sapwood parts of air-dried wood planks and conditioned at a temperature of 20  $\pm$  2 °C and 65  $\pm$  5% relative humidity until they reached an equilibrium in moisture distribution.

Melamine formaldehyde (MF), polyurethane (PUR), and polyvinyl acetate (PVAc-D4) were used as the bonding adhesives. PVAc-D4 had the following properties: density, 1.120 g/cm<sup>3</sup>; viscosity, 13000 cPs at 20 °C; pH, 7.5 at 20 °C; solid content, 50%; and hardener ratio, 5% (Turbo-Hardener 303,5, was supplied by the Aktif firm, a representative firm of Kleiberit adhesives in Istanbul, Turkey). MF had the following properties: density, 1.215 g/cm<sup>3</sup>; viscosity, 60 cPs at 20 °C; pH, 9.3 at 20 °C; and solid content, 53%. PUR had the following properties: density, 1.130 g/cm<sup>3</sup>; viscosity, 8000 mPas at 20 °C; pH, 7 at 20 °C; solid content, 100%. For all adhesives, the amount applied was 200 gr/m<sup>2</sup> (Keskin *et al.* 2003; Atar and Ozcifci 2005; Ozcifci *et al.* 2007; Sahin Kol *et al.* 2009).

### **Heat Treatment of Wood**

The samples were subjected to heat treatment at 150 °C, 175 °C, 200 °C, and 225 °C for 3 h in a heat treatment oven which was made by the Atria firm in Istanbul, controlled to within  $\pm$  1 °C under steam. The total heat treatment was performed over three continuous stages. The total time of the heat treatment was 45 h, and the duration at this high temperature was 3 h. The heat-treated and control samples were conditioned at a temperature of 20  $\pm$  2 °C and 65  $\pm$  5% relative humidity to the moisture content of about 12%. After the heat treatment, the pH value was evaluated by the extraction method. For this test, 20 g of wood was ground into small particles and soaked in 160 g of distilled water for 24 h. The extract was filtered and analyzed with a portable pH meter (Sernek *et al.* 2008).

## Preparation of Test Samples and Test Method

Weight loss

Prior to the heat treatment, samples were dried in a heating oven at  $103 \pm 2$  °C. The oven-dry weight of the samples was determined. After the heat treatment, the oven-dry weight of the same samples was re-measured. The weight loss (WL) of the samples due to the heat treatment was calculated according to the following formula,

$$WL(\%) = 100(W_{BH} - W_{AH}) / W_{BH}$$
(1)

where  $W_{BH}$  is the initial oven-dry weight of the sample prior to the heat treatment (g) and  $W_{AH}$  is the oven-dry weight of the samples after the heat treatment (g). The equilibrium moisture content (EMC) of the test samples was determined before the tests.

Density

The air-dried density of the samples was determined according to the following formula (ISO 3131 1975 and TS 2472 1976),

 $D_{12} = M_{12}/V_{12} (g/cm^3)$ 

(2)

where M is the weight of the sample (g) and V is the volume of the samples  $(cm^3)$ .

#### Bonding strength

The bonding strength was tested according to the BS EN 205 (1991) standard. The samples were cut parallel to grain in the dimensions of 5 mm  $\times$  55 mm  $\times$  500 mm. The adhesive was applied at the rate of about 200 g/m<sup>2</sup> on a single bonding surface of the veneer, as recommended by the manufacturer, with a cylindrical adhesive spreading apparatus. The wood veneer panels were pressed under 70 kg/cm<sup>2</sup> for 30 min at 120 °C for

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MF, and under 70 kg/cm<sup>2</sup> for 120 min at 20 °C and for PUR and PVAc-D4. Test samples were obtained from these panels (Fig. 1).





The test samples were conditioned at a temperature of  $20 \pm 2$  °C and  $65 \pm 5\%$  relative humidity for 30 days. During the tests, force was applied parallel to the glue line, and the loading rate was 2 mm/min. Twenty-two specimens were used for each bonding strength test. The bonding strength (BS) was calculated according to Eq. 3,

$$BS = F_{max} / a.b (N/mm^2)$$
(3)

where  $F_{\text{max}}$  is the maximum load (N), *a* is the width of the glued surface (mm), and *b* is the length of the glued surface (mm).

# **RESULTS AND DISCUSSION**

The average weight loss due to heat treatment are given in Table 1. As expected, the weight loss varied according to treatment temperature. Weight loss is attributed to the degradation of the wood polymers (hemicelluloses, cellulose, and lignin); in this temperature range, hemicelluloses are the most thermally sensitive wood components (Poncsák *et al.* 2006; Yildiz *et al.* 2006). Gunduz and Aydemir (2009) investigated the weight loss of heat-treated Camiyani black pine (*Pinus nigra* Arn. subsp. *pallasiana* var. *pallasiana*) wood at temperatures of 160 °C, 180 °C, and 200 °C for 2 h and 6 h. Their results showed that increasing the heat treatment temperature increased the weight loss of the test samples. Heat treatment reduced the pH of hornbeam wood from 5.48 to 4.05.

Heat Treatment	Weight Loss (%)	рН
Control	-	5.48
150 °C	0.96	5.02
175 °C	1.71	4.84
200 °C	4.22	4.46
225 °C	6.79	4.05

 Table 1. Average Weight Loss Values of Test Samples after Heat Treatment

The average density values of the test samples are shown in Table 2. The air-dried density values of the test samples decreased with an increase in the heat treatment temperature. The wood samples that were heat-treated at 225 °C and bonded with the PUR adhesive had the lowest air-dried density values. The weight of wood material decreases

when heat treatment is applied. The changes resulting from heat treatment could be explained by material losses in the cell wall, hemicellulose degradation into volatile products, and the evaporation of extractive substances (Korkut *et al.* 2008).

	Adhesive							
Heat Treatment	MF		PUR		PVAc-D4			
	Х		Х	sd	Х	sd		
Control	0.782	0.014	0.768	0.021	0.773	0.017		
150 °C	0.768	0.009	0.755	0.016	0.766	0.012		
175 °C	0.751	0.016	0.739	0.013	0.748	0.014		
200 °C	0.729	0.011	0.712	0.008	0.731	0.015		
225 °C	0.702	0.016	0.686	0.009	0.704	0.006		

Table 2. Density Values of Test Samples (g/cm<sup>3</sup>)

X, average value; sd, standard deviation

Table 3. Equilibrium Mo	bisture Content (EM	IC) Values of Test	Samples (%)
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	Adhesive						
Heat Treatment	reatment MF		PUR		PVAc-D4		
	Х	X sd X		sd	Х	sd	
Control	11.8	0.655	11.4	0.557	11.1	0.411	
150 °C	10.1	0.422	9.9	0.342	9.7	0.359	
175 °C	8.3	0.455	8.1	0.433	7.9	0.467	
200 °C	7.2	0.517	7.1	0.359	6.8	0.322	
225 °C	5.9	0.405	5.6	0.499	5.7	0.539	

X, average value; sd, standard deviation

The average equilibrium moisture content (EMC) values of the test samples are shown in Table 3. Heat treatment may change the wood equilibrium moisture content (EMC). According to Table 3, the EMC values of the heat-treated samples decreased with an increase in the heat treatment temperature. The treatment at 225 °C for wood bonded with the PUR adhesive sample resulted in the lowest EMC values, as previously reported (Jämsä and Viitaniemi 2001; Gosselink *et al.* 2004; Metsä-Kortelainen *et al.* 2006). Epmeier *et al.* (2001) examined the effects of heat treatment on the EMC of spruce wood. The EMC of spruce wood treated at 160 °C changed from 8.7% to 7.0% and from 18.9% to 15.7% at 30% and 90% relative humidity, respectively. The treatment at 190 °C was more effective, decreasing the EMC from 8.1% to 6.5%, and from 18.6% to 14.6% at 30% and 90% relative humidity, respectively.

The average values of the bonding strength obtained for the different adhesives and heat treatment temperatures are given in Table 4. The highest bonding strength was with the control samples, and the bonding strength of the test samples decreased with an increase in the heat treatment temperature. The lowest bonding strength values were obtained from the samples heat-treated at 225 °C (7.75 N/mm<sup>2</sup>), where the total loss compared with the control sample was 25.3%. Poncsak *et al.* (2007) studied the effects of heat treatment on the bonding strength of Scotch pine (*Pinus sylvestris*), aspen (*Populus tremuloides*), yellow poplar (*Liriodendron tulipifera*), and jack pine (*Pinus banksiana*) that were bonded with phenol resorcinol formaldehyde (PRF) and polyurethane (PUR) adhesives. The untreated

samples had a better bonding strength than the heat-treated samples. Among the three adhesives, the PUR adhesive showed the highest bonding strength (10.12 N/mm<sup>2</sup>), followed by MF (8.92, N/mm<sup>2</sup>) and PVAc-D4 (8.54 N/mm<sup>2</sup>). The bonding strength of PUR was higher than that of MF and PVAc-D4 adhesives by 11.9% and 15.6%, respectively. Percin (2012) investigated the effect of heat treatment on the bonding strength of laminated Scotch pine (*Pinus sylvestris* L.), beech (*Fagus orientalis* L.), oak (*Quercus petreae* L.), and poplar (*Populus nigra* L.) wood. The veneers were bonded with melamine formaldehyde, polyurethane, and polyvinyl acetate adhesives and then heat-treated at 185 °C or 212 °C for 2 h. The bonding strength decreased with increasing heat treatment temperature.

Varia	bles	Average Bonding Strength (N/mm <sup>2</sup> )	HG
	Control	10.38	Α
	150 °C	9.90	AB
Heat Treatment*	175 °C	9.30	AB
	200 °C	8.64	BC
	225 °C	7.75	С
	MF	8.92	В
Adhesives**	PUR	10.12	Α
	PVAc-D4	8.54	В

Table 4	. Average	Bonding	Strength	According	to Adhes	ives and	Temperatures
			. /				

\*LSD, 1.493; \*\*LSD, 1.156; HG, homogeneous group

Source of Variance	Degrees of Freedom	Sum of Square	Means of Square	F- value	Level of significance 5%
Factor A	4	282.075	70.519	3703.6055	0.0000
Factor B	2	149.000	74.500	3912.6988	0.0000
AxB	8	51.826	6.478	340.2362	0.0000
Error	315	5.998	0.019		
Total	329	488.900			

**Table 5.** Multiple Variance Analyses of Treatment Temperature and Adhesive

\*Note: Factor A is the heat treatment temperature, and Factor B is the type of adhesive

The results of multiple variance analyses tests with regard to the effects of the heat treatment temperatures and the type of adhesives are given in Table 5. The effects of heat treatment temperature and type of adhesive were found to be statistically significant for bonding strength (P < 0.05). Table 6 shows the bonding strength and the standard deviations of the untreated and heat-treated samples that were bonded with different adhesives.

The highest bonding strength was obtained in the non-heat-treated and PUR-glued wood (11.06 N/mm<sup>2</sup>), and the lowest bonding strength was obtained in the sample containing PVAc-D4 and heat-treated at 225 °C (6.13 N/mm<sup>2</sup>). The bonding strength of the heat-treated wood with the PUR adhesive was more satisfactory than that of the wood with the MF and PVAc-D4 adhesives. In addition, the bonding strength of PVAc-D4 was higher than MF in the control and heat-treated samples at 150 °C, while the bonding

strength of MF was higher than PVAc-D4 in the heat-treated samples at 175 °C, 200 °C, and 225 °C. The MF adhesive gave more satisfactory results than the PVAc-D4 at high temperatures. As shown in Table 6, the bonding strength of the heat-treated hornbeam wood decreased as the heat treatment temperature increased for the MF, PUR, and PVAc-D4 adhesives. The decreases in bonding strength were 21.7%, 15.3%, and 39.6%, respectively, compared with the control specimens. The reduction of the wood density, the properties of a heat-treated wood surface during a heat treatment, and the characteristics of adhesives used, all potentially influence the adhesive bonding performance of heat-treated hornbeam wood.

-	Adhaaiya	Value	Heat Treatment					
	Adhesive		Control	150 °C	175 °C	200 °C	225 °C	
		X (N/mm²)	9.93	9.31	9.01	8.58	7.78	
	MF	sd	0.1033	0.1041	0.1392	0.1329	0.1071	
		HG	AB	AB	AB	ABC	BC	
		X (N/mm²)	11.06	10.63	10.01	9.53	9.37	
	PUR	sd	0.1394	0.1024	0.1436	0.1766	0.1451	
		HG	А	А	AB	AB	AB	
	PVAc-D4	X (N/mm²)	10.15	9.77	8.87	7.81	6.13	
		sd	0.1725	0.1172	0.1339	0.1571	0.1462	
		HG	AB	AB	AB	BC	С	

**Table 6.** Average Bonding Strength According to the Interaction of Adhesive and

 Treatment Temperature

\*LSD, 2.585; X, average bonding strength; HG, homogeneous group; sd, standard deviation

Moreover, the amount of adhesive penetration into a wood surface plays a vital role in the bond performance (Kamke and Lee 2007). Sogutlu and Dongel (2007) reported that the bonding strength of higher density wood is higher than that of lower density wood. The surface wettability is an important factor for good adhesion during wood bonding. Due to the less hygroscopic (hydrophobic) and less polar properties of heat-treated wood, the distribution of the adhesive on the surface and the penetration of the adhesive into the wood structure can be affected (Paul *et al.* 2007; Sernek *et al.* 2007, 2008).

There is evidence supporting the positive relationship between wood wettability and adhesion (Wellons 1977). The wettability of heat-treated spruce and pine wood shows similar behavior, with a decrease in the wettability at treatment temperatures between 100  $^{\circ}$ C and 160  $^{\circ}$ C (Hakkou *et al.* 2005). In addition, heat treatment reduces the pH of hornbeam wood due to the production of acetic and formic acids. The pH of wood can influence the hardening of an adhesive, which might either retard or accelerate the adhesive curing, depending on the adhesive used for bonding (Kariz and Sernek 2010).

Dilik and Hiziroglu (2012) investigated the effect of heat treatment and compression on bonding strength of Eastern red cedar (*Juniperus virginiana*) wood. Test samples were exposed to 120 °C, 160 °C, and 190 °C for 6 h before they were compressed using 2.5 MPa pressure for 5 min and bonded with polyvinyl acetate (PVAc) adhesive. Test results showed that the bonding strength of samples decreased with increasing heat treatment temperature. Chow (1971) examined the bonding performance of phenol-formaldehyde glue (PF) bonded heat treated veneers. The results showed that there was a

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reduction in the bonding strength as the temperature and treatment duration increased. The bonding quality of heat- treated wood changes due to the reduction of surface energy, which affects the wettability of the wood material. Also, bonded heat-treated at 180 °C, 200 °C, and 220 °C aspen, beech, maple, and elm woods with a UF adhesive. There was a decrease in the shear strength of the adhesive line with increasing temperature and duration of treatment (Chang and Keith 1978).

# CONCLUSIONS

- 1. Non-treated hornbeam wood showed highest bonding strength, while the samples bonded with the polyurethane (PUR) adhesive showed a higher bonding strength compared to the others considered.
- 2. The lowest average reduction values in bonding strength of the test specimens was determined for specimens exposed 150 °C heat treatment.
- 3. The bonding strength of heat-treated wood specimens decreased after the heat treatment. The highest bonding strengths of the melamine formaldehyde (MF), PUR, and polyvinyl acetate (PVAc-D4) adhesives were observed for the control specimens (9.93, 11.06, and 10.15 N/mm<sup>2</sup>, respectively), whereas the lowest strength was observed for the heat-treated specimens at 225 °C (7.78, 9.37, and 6.11 N/mm<sup>2</sup>, respectively).
- 4. Considering the three adhesives used, the PUR adhesive showed the greatest bonding strength, followed by the MF and PVAc-D4 adhesives. Bonding strength of all adhesive types decreased with increasing of the heat treatment temperature. Therefore, the lower heat treatment temperature and surface modification methods should be used in order to reach the highest bonding strength.

# **REFERENCES CITED**

- Atar, M., and Ozcifci, A. (2005). "On the bonding strength of laminated wood materials produced from European beech (*Fagus sylvatica*) and scots pine (*Pinus sylvestris* L.) glued with polyvinyl acetate (PVAc)-D4 adhesive," *Jestech* 8(4), 305-310.
- BS EN 205 (1991). "Test methods for wood adhesives for non-structural applicationsdetermination of tensile shear strength of lap joints," British Standards Institution, London, UK.
- Chang, C. I., and Keith, C. T. (1978). Properties of Heat-Darkened Wood: II. Mechanical Properties and Gluability (Report No. OPX214E), Eastern Forest Products Laboratory, Ottawa, Canada, pp. 1-19.
- Chow, S. Z. (1971). "Infrared spectral characteristics and surface inactivation of wood at high temperatures," *Wood Science Technology* 5, 27-39. DOI: 10.1007/BF00363118.
- Dilik, T., and Hiziroglu, S. (2012). "Bonding strength of heat treated compressed Eastern red cedar wood," *Materials & Design* 42, 317-320. DOI: 10.1016/j.matdes.2012.05.050
- Demirkir, C., Özsahin, Ş., Aydin, I., and Colakoglu, G. (2013). "Optimization of some panel manufacturing parameters for the best bonding strength of plywood,"

International Journal of Adhesion and Adhesives 46(10), 14-20. DOI: 10.1016/j.ijadhadh.2013.05.007.

- Epmeier, H., Bengtsson, C., and Westin, M. (2001). "Effect of acetylation and heat treatment on dimensional stability and MOE of spruce timber," in: *Proceedings for the First Conference of the European Society for Wood Mechanics*, Lausanne, Switzerland.
- Esen, R. and Ozcan, C. (2012). "The effects of heat treatment on shear strength of oak (*Quercus petraea* L.) wood," *SDU Faculty of Forestry Journal* 13(2), 150-154.
- Esteves, B. and Pereira, H. (2009). "Wood modification by heat treatment: A review," *BioResources* 4(1), 370-404. DOI: 10.15376/biores.4.1.370-404
- Fengel, D. and Wegener, G. (1984). *Wood, Chemistry, Ultrastructure, Reactions*, Waster & Grugter, New York, NY, USA.
- Gosselink, R. J. A., Krosse, A. M. A., Van der Putten, J. C., Van der Kolk, J. C., De Klerk-Engels, B., and Van Dam, J. E. G. (2004). "Wood preservation by lowtemperature carbonization," *Industrial Crops and Products* 19(1), 3-12. DOI:10.1016/S0926-6690(03)00037-2.
- Gunduz, G., and Aydemir, D. (2009). "The influence of mass loss on the mechanical properties of heat-treated black pine wood," *Wood Research* 54(4), 33-42.
- Hakkou, M., Pétrissans, M., El Bakali, I., Gérardin, P., and Zoulalian, A. (2005).
  "Wettability changes and mass loss during heat treatment of wood," *Holzforschung* 59(1), 35-37. DOI: 10.1515/HF.2005.006.
- ISO 3131 (1975). "Wood-Determination of density for physical and mechanical tests," International Organization for Standardization, Geneva, Switzerland.
- Jämsä, S. and Viitaniemi, P. (2001). "Heat treatment of wood-better durability without chemicals," in: *Proceedings of Special Seminar*, Antibes, France.
- Johansson, D. (2008). *Heat Treatment of Solid Wood: Effects on Absorption, Strength, and Colour*, Ph.D. Dissertation, Luleå University of Technology LTU, Skelleftea, Sweden.
- Kamke, F. A., and Lee, J. N. (2007). "Adhesive penetration in wood: A review," *Wood and Fiber Science* 39(2), 205-220.
- Kariz, M., and Sernek, M. (2010). "Bonding of heat-treated spruce with phenol formaldehyde adhesive," *Journal of Adhesion Science and Technology* 24(8), 1703-1716. DOI: 10.1163/016942410X507768.
- Keskin, H., Atar, M., and Kurt, R. (2003). "Physical and mechanical properties of the laminated scots pine (*Pinus sylvestris* L.) wood," *KSU Journal of Science and Engineering* 6(1),75-84.
- Korkut, D. S., Korkut, S., Bekar, I., Budakçi, M., Dilik, T., and Çakicier, N. (2008). "The effects of heat treatment on the physical properties and surface roughness of Turkish hazel (*Corylus colurna* L.) wood," *International Journal of Molecular Science* 9(9), 1772-1783. DOI:10.3390/IJMS9091772.
- Korkut, S. (2007). "The effects of heat treatment on some technological properties in Uludağ fir (*Abies bornmuellerinana* Mattf.) wood," *Building and Environment* 43(4), 422-426. DOI:10.1016/j.buildenv.2007.01.004.
- Metsä-Kortelainen, S., Antikainen, T., and Viitaniemi, P. (2006). "The water absorption of sapwood and heartwood of Scots pine and Norway spruce heat-treated at 170 °C, 190 °C, 210 °C, and 230 °C," *Holz als Roh-und Werkstoff* 64, 192-197. DOI: 10.1007/s00107-005-0063-y

- Militz, H. (2002). "Thermal treatment of wood, European processes, and their background," *International Research Group on Wood Protection*, No: IRG/WP 02-40241.
- Nuopponen, M., Vuorinen, T., Jamsä, S., and Viitaniemi, P. (2004). "Thermal modifications in softwood studied by FTIR and UV resonance Raman spectroscopies," *Journal of Wood Chemistry and Technology* 24(1), 13-26. DOI: 10.1081/WCT-120035941
- Ozcifci, A., Toker, H., and Baysal, E. (2007). "Fire properties of laminated veneer lumber treated with some fire retardants," *Wood Research* 52(4), 37-46.
- Paul, W., Ohlmeyer, M., and Leithoff, H. (2007). "Thermal modification of OSB-strands by a one-step heat pretreatment-Influence of temperature on weight loss, hygroscopicity, and improved fungal resistance," *Holz Roh Werkst* 65, 57-63. DOI: 10.1007/s00107-006-0146-4.
- Pavlo, B. and Niemz, P. (2003). "Effect of temperature on color and strength of spruce wood," *Holzforschung* 57(5), 539-546.
- Percin, O. (2012). Investigation of the Effects of on Some Technological Properties of Heat Treatment of the Laminated Wood Material, Ph.D. Dissertation, Gazi University, Ankara, Turkey.
- Percin, O. and Uzun, O. (2014). "Determination of bonding strength in heat treated some wood materials," *SDU Faculty of Forestry Journal* 15(1), 72-76.
- Poncsák, S., Shi, S. Q., Kocaefe, D., and Miller, G. (2007). "Effect of thermal treatment of wood lumbers on their adhesive bond strength and durability," *Journal of Adhesion Science and Technology* 21(8), 745-754. DOI:10.1163/156856107781362653.
- Poncsák, S., Kocaefe, D., Bouazara, M., and Pichette, A. (2006). "Effect of high temperature treatment on the mechanical properties of birch (*Betula papyrifera*)," *Wood Science and Technology* 40(8), 647-663. DOI: 10.1007/s00226-006-0082-9.
- Sahin Kol, H., Ozbay, G., and Altun, S. (2009). "Shear strength of heat-treated tali (*Erythrophleum ivorense*) and Iroko (*Chlorophora excelsa*) woods, bonded with various adhesives," *BioResources* 4(4), 1545-1554.
- Sernek, M., Humar, H., Kumer, M., and Pohleven, F. (2007). "Bonding of thermally modified spruce with PF and UF adhesives," in: *Proceedings of the 5<sup>th</sup> COST E34 International Workshop*, Bled, Slovenia, pp. 31-39.
- Sernek, M., Boonstra, M., Pizzi, A., Despres, A., and Gérardin, P. (2008). "Bonding performance of heat treated wood with structural adhesives," *Holz als Roh- und Werkstoff* 66(3), 173-180. DOI: 10.1007/s00107-007-0218-0.
- Sivonen, H., Maunu, S., Sundholm, F., Jämsä, S., and Viitaniemi, P. (2002). "Magnetic resonance studies of thermally modified wood," *Holzforschung* 56(6), 648-654. DOI: 10.1515/HF.2002.098.
- Sogutlu, C., and Dongel, N. (2007). "Tensile shear strengths of some local woods bonded with polyvinyl acetate and polyurethane adhesives," *Journal of Polytechnic* 10(3), 287-293. DOI: 10.2339/2007.10.3.287-293.
- Tjeerdsma, B. F., Boonstra, M., Pizzi, A., Tekely, P., and Militz, H. (1998).
  "Characterization of thermally modified wood: Molecular reasons for wood performance improvement," *Holz als Roh- und Werkstoff* 56(3), 149-153. DOI: 10.1007/s001070050287.
- TS 2472 (1976). "Wood- determination of density for physical and mechanical tests," Turkish Standards Institution, Ankara, Turkey.

- Wellons, J. D. (1977). "Adhesion to wood substrates," in: ACS Symposium Series, R. F. Gould, (ed.), American Chemical Society, Washington, DC, USA, pp. 150-168.
- Yıldız, S., Gezer, E. D., and Yıldız, U. C. (2006). "Mechanical and chemical behavior of spruce wood modified by heat," *Building and Environment* 41(12), 1762-1766. DOI:10.1016/J.Buildenv.2005.07.017.
- Yorur, H., Kurt, Ş., and Uysal, B. (2014). "Bonding strength of oak with different adhesives after humid-water-heat tests," *Journal of Adhesion Science and Technology* 28(7), 690-701. DOI: 10.1080/01694243.2013.860676.

Article submitted: March 24, 2016; Peer review completed: July 10, 2016; Revised version received and accepted: July 16, 2016; Published: July 22, 2016. DOI: 10.15376/biores.11.3.7686-7696