Propagation Velocity Model of Stress Waves in Larch Wood (*Larix gmelinii*) Three-dimensional Space with Different Moisture Contents

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Based on the effects of stress wave propagation in larch (Larix gmelinii) wood, the propagation mechanism of stress wave was explored, and a theoretical model of the propagation velocity of stress waves in the threedimensional space of wood was developed. The cross and longitudinal propagation velocities of stress wave were measured in larch wood under different moisture contents (46% to 87%, 56% to 96%, 20% to 62%, and 11% to 30%) in a laboratory setting. The relationships between the propagation velocity of stress waves and the direction angle or chord angle with different moisture contents were analyzed, and the three-dimensional regression models among four parameters were established. The analysis results indicated that under the same moisture content, stress wave velocity increased as the direction angle increased and decreased as chord angle increased, and the radial velocity was the largest. Under different moisture contents, stress wave velocity gradually decreased as moisture content increased, and the stress wave velocity was more noticeably affected by moisture content when moisture content was below the fiber saturation point (FSP, 30%). The nonlinear regression models of the direction angle, chord angle, moisture content, and the propagation velocity of stress wave fit the experiment data well ($R^2 \ge 0.97$).

Keywords: Stress waves; Moisture content; Three-dimensional space; Propagation velocity model

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INTRODUCTION

Stress waves are an important nondestructive tool for evaluating the quality and predicting the strength of wood. Stress wave detection is based on the relationships between sound propagation velocity (v), wood density (ρ), and elastic modulus (E) in wood (Randow and Gazonas 2009; Xu *et al.* 2018; Simic *et al.* 2019). Stress wave generation uses a pulse hammer to strike the transmitter sensor on the tested wood so that a mechanical stress wave is generated inside the wood and propagates under stress, and propagation time is measured by specific equipment to determine the elastic modulus of the wood (Feng-Lu *et al.* 2016; Liao *et al.* 2017).

Wood is hygroscopic, heterogeneous, and anisotropic. The propagation of stress waves in wood is affected by tree species, moisture content, and environmental temperature (Chauhan and Walker 2006; Chan *et al.* 2011; Liu *et al.* 2014; Yang *et al.* 2015). Xu *et al.* (2011) studied the effects of moisture content and temperature on the propagation velocity of stress waves in Korean pine wood. The work showed that moisture content is an important factor affecting stress wave propagation, and a regression model was established

between the propagation velocity of stress wave and moisture content. Liu and Gao (2014) examined the longitudinal stress wave velocities of wood samples in different radial locations with different moisture content (0% to 65%). Yamasaki *et al.* (2017) investigated the effect of moisture content on the stress wave propagation velocity and obtained the relationship between the moisture content and the rate of change of velocity of full-size timber. This relationship was used to estimate the Young's modulus of the timber in the air-drying state from the velocity in high-moisture condition. Yue *et al.* (2018) investigated on the effects of the seasonal temperature and moisture content on the electrical resistance of standing trees, and their combined effects on electrical resistance were analyzed, following which a regression model was also established. Cheng *et al.* (2020) developed a set of reformulated theoretical formulas to measure the relationships between moisture content and stress wave propagation velocity, dynamic modulus of elasticity (*E*_d), and modulus of stress-resistograph of the wood. The formulas can be used to quickly get the change trend of wood properties, and the calculated results were consistent with the experimental data.

In recent years, the theoretical model of stress wave propagation in wood has been thoroughly studied. Zhang *et al.* (2016) studied the propagation mechanism of stress waves in the cross-section and longitudinal section of *Pinus resinosa* and identified the time contour curve of stress wave propagation in standing trees. Li *et al.* (2014) examined stress wave velocity patterns in the cross-sections of black cherry trees, developed analytical models of stress wave velocity in healthy trees, and then tested the effectiveness of the models as a tool for tree decay diagnosis. Weng *et al.* (2016) established the propagation velocity model of stress wave in the radial section of wood and designed a four-way cross detection method to detect the internal defects of trees.

This study aimed to investigate stress wave propagation velocity in threedimensional space with different moisture contents. Using the stress wave propagation velocity patterns in the cross and longitudinal sections of healthy trees as the foundation of the physical and mechanical properties of wood, a theoretical model of stress wave propagation velocity was obtained for different space angles, and the effect of moisture content on stress wave velocity of larch wood in different direction angles and chord angles was explored. In addition, regression models of stress wave propagation velocity, direction angle, chord angle, and moisture content in larch wood were established.

Theoretical Analysis of Stress Wave Propagation Velocity Model in Wood

Fibre direction influences many of the physical properties of wood. Among others, the electrical and thermal conductivity, swelling and shrinking, and the strength and stiffness properties strongly depend on the considered orientation relative to the fibre direction (Ehrhart *et al.* 2017; Liu *et al.* 2019). Wood is anisotropic, and in wood segments free of knots, bark inclusions, or any other local defect, wood is an approximately cylindrical material using the three main directions (longitudinal (L), tangential (T), and radial (R)) (Fig. 1).

Stress waves are assumed to propagate in the *SE* direction in the *LR* plane as shown in Fig. 1(b), in which *S* represents the signal transmitter and *E* represents the signal receiver. Given the angle (β) between *SR* and *SE*, *i.e.*, the direction angle, it is positive downward and negative upward. According to Hankinson's wood diagonal compressive strength formula, the relationship between stress wave propagation velocity (*V*) and direction angle (β) was calculated with Eq. 1 (Mascia *et al.* 2011),

$$V(\beta) = v_1 v_r / (v_1 cos^2 \beta + v_r sin^2 \beta)$$
⁽¹⁾

where $V(\beta)$ is the propagation velocity (m/s) of stress wave in *LR* plane, v_1 is longitudinal velocity (m/s), and v_r is radial velocity (m/s). Equation 1 was approximated with the second-order Taylor polynomial, and the remainder was removed to obtain Eq. 2:

$$V(\beta) \approx v_{\rm r} + v_{\rm r}(1 - v_{\rm r}/v_{\rm l})\beta^2 \tag{2}$$



Fig. 1. The cylindrical anisotropy of wood and the wood main directions longitudinal (L), tangential (T), and radial (R) on a wood plane (a); stress wave propagation in the LR plane (b) and the TR plane (c)

As shown in Fig. 1c, *S* represents the signal transmitter, *F* represents the signal receiver, the angle between *SR* and *SF* is expressed by α , clockwise is negative, and counterclockwise is positive. The *TR* plane is considered a regular circle, and the stress wave propagates in the direction of *SF*. The propagation velocity in the *SR* direction is the radial velocity ($\alpha = 0$), and the propagation velocity in the other directions is called chord velocity. According to Dikrallah *et al.* (2006), the acoustic anisotropy of wet wood was analyzed *via* a guided wave experiment, and the propagation of stress waves in the cross-section of wood was studied. The mathematical relationship between stress wave propagation velocity (*V*) and the chord angle α was obtained with Eq. 3,

$$V(\alpha) = v_R \cos^2 \alpha \sqrt{1 + \frac{E_T}{E_R} \tan^4 \alpha + 2\frac{G_{RT}}{E_R} \tan^2 \alpha}$$
(3)

where $V(\alpha)$ is the propagation velocity of stress wave in *TR* plane, v_R is radial velocity ($\alpha = 0$), and E_T , E_R , and G_{RT} represent the radial modulus of elasticity, tangential modulus of elasticity, and shear modulus, respectively.

According to Eq. 3, $V(0) = v_R$, V'(0) = 0, $V''(0) = -2v_R(1 - G_{RT}/E_R)$, and the function $V(\alpha)$ could be expanded to Taylor series at $\alpha = 0$ with Eq. 4:

$$V(\alpha) = v_{\rm R}[1 - (1 - G_{\rm RT}/E_{\rm R})\alpha^2]$$
(4)



Fig. 2. The propagation diagram of stress wave in three-dimensional coordinate system of wood

In cylindrical wood, a three-dimensional coordinate system was established with S as the origin, as shown in Fig. 2. The propagation velocities of stress wave, such as v_r , v_l , v_R , $V(\beta)$ and $V(\alpha)$ are represented in vector form in three-dimensional coordinate system. The $V(\alpha)$ of Eq. 4 is the v_r of Eq. 2, and Eq. 4 is substituted into Eq. 2. Let $f(\alpha, \beta)$ represent the simplified formula; the propagation velocity model of stress waves in three-dimensional space was obtained with Eq. 5:

$$f(\alpha,\beta) = v_{r} + v_{r}(1 - \frac{v_{r}}{v_{l}})\beta^{2}$$

$$= v_{R}[1 - (1 - \frac{G_{RT}}{E_{R}})\alpha^{2}] + v_{R}[1 - (1 - \frac{G_{RT}}{E_{R}})\alpha^{2}] \left\{ 1 - \frac{v_{R}[1 - (1 - \frac{G_{RT}}{E_{R}})\alpha^{2}]}{v_{l}} \right\}\beta^{2}$$

$$= v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2} + [v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2}] \left\{ \beta^{2} - \frac{v_{R}[1 - (1 - \frac{G_{RT}}{E_{R}})\alpha^{2}]\beta^{2}}{v_{l}} \right\}$$

$$= v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2} + [v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2}] \left[(1 - \frac{v_{R}}{v_{l}})\beta^{2} + (\frac{v_{R}}{v_{l}} - \frac{v_{R}G_{RT}}{v_{l}E_{R}})\alpha^{2}\beta^{2} \right]$$

$$= v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2} + [v_{R} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2}] \left[(1 - \frac{v_{R}}{v_{l}})\beta^{2} + (\frac{v_{R}}{v_{l}} - \frac{v_{R}G_{RT}}{v_{l}E_{R}})\alpha^{2}\beta^{2} - (1 - \frac{G_{RT}}{E_{R}})v_{R}\alpha^{2} + (1 - \frac{v_{R}}{v_{l}})v_{R}\beta^{2} + (2\frac{v_{R}^{2}}{v_{l}} - 2\frac{v_{R}^{2}G_{RT}}{v_{l}E_{R}} - v_{R} + \frac{v_{R}G_{RT}}{E_{R}})\alpha^{2}\beta^{2} - (1 - \frac{G_{RT}}{E_{R}})v_{R}(\frac{v_{R}}{v_{l}} - \frac{v_{R}G_{RT}}{v_{l}E_{R}})\alpha^{2}\beta^{2} - (1 - \frac{G_{RT}}{E_{R}})v_{R}(\frac{v_{R}}{v_{l}} - \frac{v_{R}G_{RT}}{v_{l}E_{R}})\alpha^{4}\beta^{2}$$

When wood is approximately cylindrical, the propagation velocity $f(\alpha, \beta)$ is the sum of polynomials with the highest degree of 4 in direction angle (β) and chord angle (α), and

it is symmetric about $\alpha = 0$, $\beta = 0$. To simplify the theoretical model, the high-order terms in the formula were ignored, and the simplified formula (Eq. 6) was used:

$$f(\alpha,\beta) \approx v_{\rm R} + (1 - v_{\rm R}/v_{\rm I})v_{\rm R}\beta^2 - (1 - G_{\rm RT}/E_{\rm R})v_{\rm R}\alpha^2 \tag{6}$$

In this paper, Eq. 6 was used as the basic model for the propagation velocity of stress waves in the three-dimensional space of healthy wood. The α and β values were used to determine the specific direction of stress wave propagation in wood space, and the G_{RT} and E_R values were determined by the mechanical properties of wood itself, which were obtained according to different wood species. The v_R and v_I were obtained by experimental measurement.

However, moisture content notably affects the propagation velocity of stress waves in wood, and the stress wave propagation velocity decreases gradually as moisture content increases (Gao *et al.* 2017). When the moisture content was introduced into the basic model (Eq. 6) as a variable, a more complete model of the propagation velocity of the stress wave in the three-dimensional space was established to obtain a more accurate space propagation velocity of the larch wood.

EXPERIMENTAL

Materials

Larch (*Larix gmelinii*) was obtained from the experimental forest farm of Northeast Forestry University (Harbin, China). Samples were selected that were free of nodes, decay, and cracking, they were felled, and branches were subsequently removed. Four 0.7-m-long wood pieces were cut from four sample trees of uniform thickness at a height of 0.6 m above the ground, and the diameter at breast height (DBH) values of the specimens were 20 cm, 22 cm, 22 cm, and 23 cm. The four 0.7-m-long wood specimens were numbered (#1, #2, #3, and #4) and immediately sealed in plastic wrap. Next, the wood specimens were directly transported to the mechanics laboratory of Northeast Forestry University and kept in a conditioned room at 20 $^{\circ}$ C.

Methods

Stress wave velocity measurement

Twelve test positions were selected on both sides of the longitudinal sections on each of the larch specimens at intervals of 10 cm. Pins were fixed onto each test position, and the pins were numbered No. 1 to No. 12. The nondestructive stress wave tester (Arbotom, Frank Rinn, Germany) was used to measure the stress wave velocity. The sensors were attached at the pins of each sample. After striking the sensors on one side, the transmitted stress wave was detected by the sensors on the other side of each specimen, and the direction angle between the contralateral sensors was represented by β . Then, sensors No. 1 to No. 6 were fixed, and sensors No. 7 to No. 12 were changed so that the angle between the longitudinal section and the radial section was expressed by α . The values of α were $0, \pm 15^{\circ}, \pm 30^{\circ}, \pm 45^{\circ}, \pm 60^{\circ}$, and $\pm 75^{\circ}$, and the stress wave velocities in 11 different longitudinal sections were measured; the same longitudinal section was measured 5 times and averaged. The equipment for stress wave testing is shown in Fig. 3



Fig. 3. Schematic diagram of nondestructive stress wave testing of wood

Moisture content measurement

The volume of wood specimens is relatively large. A high frequency wood moisture meter (FD-100B; Shanghai Yuanqi Testing Instrument Co., Ltd., Shanghai, China) was used to quickly determine the moisture content of samples, and the measurement range was 0 to 100%. The initial moisture contents of the samples (#1, #2, #3, and #4) were estimated using the direct measurements taken by the moisture meter, and then samples #1 and #2 were immersed in water to improve their moisture contents. Samples were then taken at 5 intervals to measure the moisture content and the stress wave propagation velocity. Samples #3 and #4 were dried in a self-made experimental drying kiln of Northeast Forestry University, which could detect the moisture content of the wood samples in real time. When the moisture content reached the preset value, the samples were taken out to verify the moisture content with an FD-100B and measure the propagation velocity of the stress wave. The samples were also taken out 5 times and recorded during this part of the experiment. The measured moisture contents of the samples (#1, #2, #3, and #4) are shown in Table 1.

Sample Number	Moisture Content (%)					
#1	46	52	59	78	87	
#2	56	66	72	84	96	
#3	20	32	41	50	62	
#4	11	16	22	26	30	

Table 1. Sample Moisture Content Measurement

Statistical analysis method

Based on the measured data, drawing software (Origin, OriginLab, v.9.0, Northampton, MA, USA) and statistical analysis software (SPSS, IBM, IBM SPSS Statistics 26.0, Armonk, NY, USA) were used to analyze the propagation velocity of stress wave in the longitudinal section and the cross-section with different moisture contents, and establish the corresponding regression model. Matlab software (MATLAB, MathWorks, MATLAB R2017b, Natick, MA, USA) was used to analyze the comprehensive influence law of stress wave propagation velocity in different moisture contents and space angles and draw three-dimensional curved surface.

RESULTS AND DISCUSSION

Analysis of the Longitudinal Section Velocity of Stress Wave with Different Moisture Contents

When the chord angle (α) of larch was 0, the propagation velocity of the stress waves at different direction angles (β) between sensor No. 3 and sensors No.7 to No.12 were measured on the wood samples (#1, #2, #3, and #4) with different moisture contents. The results are shown in Fig. 4.





Fig. 4. Effect of direction angle on stress wave velocity with (a) 46% to 87% moisture contents, (b) 56% to 96% moisture contents, (c) 20% to 62% moisture contents, and (d) 11% to 30% moisture contents

Figure 4 shows that when the moisture content of larch wood samples was different, the effects of directional angle change on the propagation velocity of stress wave were similar. When the propagation velocity increased with increasing direction angle, the horizontal or radial ($\alpha = 0$) velocity was the smallest, and the overall trend was an upward parabola from the opening that was symmetrical about 0. The propagation velocity of the stress wave gradually decreased as moisture content increased, and at the moisture content of approximately 30%, the propagation velocity changed greatly (Fig. 4), and the stress wave velocity was more noticeably affected by moisture content when moisture content was below 30%.

Table 2. Regression Analysis between	 Stress Wave 	Velocity and	Direction	Angle
with Different Larch Moisture Contents	\$			

	#1	#2				
Moisture	Regression Model	R ²	Moisture	Regression Model F		
Content	$y = Ax^2 + C$		Content	$y = Ax^2 + C$		
46%	$y = 0.043x^2 + 3308$	0.96	56%	$y = 0.047x^2 + 3238$	0.96	
52%	$y = 0.052x^2 + 3262$	0.96	66%	$y = 0.044x^2 + 3192$	0.95	
59%	$y = 0.044x^2 + 3231$	0.97	72%	$y = 0.053x^2 + 3154$	0.90	
78%	$y = 0.054x^2 + 3120$	0.95	84%	$y = 0.048x^2 + 3094$	0.93	
87%	$y = 0.047x^2 + 3080$	0.93	96%	$y = 0.040x^2 + 3048$	0.89	
	#3		#4			
Moisture	Regression Model	R ²	Moisture	Regression Model	R ²	
Content	$y = Ax^2 + C$		Content	$y = Ax^2 + C$		
20%	$y = 0.049x^2 + 4010$	0.98	11%	$y = 0.047x^2 + 4400$	0.92	
32%	$y = 0.048x^2 + 3372$	0.92	16%	$y = 0.049x^2 + 4198$	0.94	
41%	$y = 0.059x^2 + 3313$	0.95	22%	$y = 0.049x^2 + 3935$	0.97	
50%	$y = 0.055x^2 + 3270$	0.93	26%	$y = 0.052x^2 + 3750$	0.94	
62%	$y = 0.048x^2 + 3204$	0.88	30%	$y = 0.042x^2 + 3604$	0.93	

The fiber saturation point (FSP) is an important concept in wood-moisture relations. The FSP can be defined as the moisture content of wood when only the bound water in cell wall reaches saturation, but there is no free water in cell cavity and intercellular space. It was an important boundary point for the changes in wood physical and mechanical properties (Stamm 1929; Skaar 1988). Below the FSP, there was no free water in the cell cavity of wood, whereas almost all the changes of physical and mechanical properties of wood mainly occur in the change stage of bound water content in the cell wall, and the drying shrinkage and swelling of wood basically depend on the change of bound water content. Above the FSP, the bound water and free water coexist. Thus, the composition of wood includes the free water and wood body with the fiber saturation point. The change of water content was the increase or decrease of free water in the cell cavity, which has no effect on the physical properties of wood except for its mass (Gao and Wang 2008). At present, the FSP commonly used in most textbooks is 23% to 33%, with an average of 30% (Gao et al. 2019). The propagation velocity of stress wave in wood is affected by the physical and mechanical properties of wood. Therefore, FSP is also an important boundary point that affects the change of stress wave velocity.

SPSS software was used to conduct regression analysis on the data of stress wave velocity and direction angle according to the mathematical model ($y = Ax^2 + C$) of Eq. 2, and regression models between them were established (Table 2). For all moisture contents of the larch wood samples, the regression curve of stress wave velocity and direction angle satisfied the one-dimensional quadratic function relation, and the determination coefficients (R^2) were above 0.88, which indicated that the models had high relation.

Analysis of the Cross-section Velocity of Stress Wave with Different Moisture Contents

When the direction angle β of larch was 0, the propagation velocity of the stress waves of different chord angles α were measured on the wood samples (#1, #2, #3, and #4) with different moisture content. The results are shown in Fig. 5.





Fig. 5. Effect of chord angle on stress wave velocity with (a) 46% to 87% moisture contents, (b) 56% to 96% moisture contents, (c) 20% to 62% moisture contents, and (d) 11% to 30% moisture contents

	#1	#2				
Moisture	Regression Model R ²		Moisture	Regression Model	R ²	
Content	$y = Ax^2 + C$		Content	$y = Ax^2 + C$		
46%	$y = -0.051x^2 + 3310$	0.96	56%	$y = -0.056x^2 + 3256$	0.97	
52%	$y = -0.051x^2 + 3280$	0.97	66%	$y = -0.054x^2 + 3194$	0.95	
59%	$y = -0.053x^2 + 3264$	0.96	72%	$y = -0.055x^2 + 3163$	0.95	
78%	$y = -0.052x^2 + 3150$	0.94	84%	$y = -0.054x^2 + 3115$	0.93	
87%	$y = -0.048x^2 + 3081$	0.95	96%	$y = -0.052x^2 + 3023$	0.91	
	#3		#4			
Moisture	Regression Model	R ²	Moisture	Regression Model	R ²	
Content	$y = Ax^2 + C$		Content	$y = Ax^2 + C$		
20%	$y = -0.053x^2 + 4022$	0.94	11%	$y = -0.042x^2 + 4386$	0.93	
32%	$y = -0.442x^2 + 3368$	0.96	16%	$y = -0.039x^2 + 4162$	0.94	
41%	$y = -0.047x^2 + 3325$	0.95	22%	$y = -0.040x^2 + 3914$	0.97	
50%	$y = -0.050x^2 + 3280$	0.94	26%	$y = -0.043x^2 + 3755$	0.87	
62%	$y = -0.047x^2 + 3197$	0.92	30%	$y = -0.043x^2 + 3577$	0.97	

Table 3. Regression Analysis between Stress Wave Velocity and Chord Angle

 with Different Larch Moisture Contents

Figure 5 shows that the effects of the variation of chord angle on the stress wave velocity of larch wood samples with different moisture content were similar. The stress wave propagation velocity decreased as chord angle increased, and the radial propagation velocity was the largest. The overall trend was a downward parabola from the opening that was symmetrical about 0. Similarly, the propagation velocity decreased as the moisture content in the cross-sections increased, and the variation range of moisture content above the FSP was smaller than that below the FSP. For the regression analysis shown in Table 3, in accordance with the mathematical model ($y = Ax^2 + C$) of Eq. 4, the determination coefficients (\mathbb{R}^2) were above 0.87, which indicated that the models had high relation.

A stress wave, as an elastic mechanical wave, has different propagation velocity in different directions of the same tree species when it propagates in wood. When the tree rings were uniform, the material is dense and the texture is straight, the cut material is uniform, and the tubular cells are arranged neatly and straightly, which is beneficial to the propagation of elastic waves, that is, the stress wave propagates fastest in the direction of the same wood, and the radial propagation velocity under the transverse stripes is greater than the chord propagation velocity.

Analysis of the Three-dimensional Velocity of Stress Wave with Different Moisture Contents

The comprehensive influence of stress wave propagation velocity of the samples #1 and #4 with different moisture contents and space angles are shown in Fig. 6. The threedimensional surface maps showed that the interaction between the direction angle, chord angle, and moisture content had a great influence on the stress wave velocity, and the propagation velocity of the stress wave propagated symmetrically with the direction angle and the chord angle. Under different moisture contents, the regression models of stress wave propagation velocity and space angles were established according to the mathematical model ($z = Ax^2 + By^2 + C$) of Eq. 6. As the R² coefficients were above 0.97 and the significance (P) was less than 0.01, the models had high relation. Analysis of the models showed that variation in moisture content had small effects on coefficients A and B and had a large effect on C.



Fig. 6. The comprehensive influence of stress wave propagation velocity for different space angles of (a) 11% to 30% moisture contents, (b) 46% to 87% moisture contents

Table 4. Regression Analysis between	Stress Wave Velocity and Space Angles
with Different Larch Moisture Contents	i de la construcción de la constru

Moisture Content	Regression Model $z = Ax^2 + By^2 + C$	R ²	Р				
11%	$z = 0.048x^2 - 0.044y^2 + 4392$	0.97	< 0.01				
16%	$z = 0.049x^2 - 0.043y^2 + 4179$	0.97	< 0.01				
22%	$z = 0.049x^2 - 0.043y^2 + 3925$	0.99	< 0.01				
26%	$z = 0.050x^2 - 0.045y^2 + 3754$	0.95	< 0.01				
30%	$z = 0.046x^2 - 0.044y^2 + 3591$	0.98	< 0.01				
46%	$z = 0.046x^2 - 0.050y^2 + 3314$	0.97	< 0.01				
52%	$z = 0.051x^2 - 0.040y^2 + 3272$	0.98	< 0.01				
59%	$z = 0.045x^2 - 0.050y^2 + 3248$	0.97	< 0.01				
78%	$z = 0.049x^2 - 0.049y^2 + 3133$	0.97	< 0.01				
87%	$z = 0.048x^2 - 0.048y^2 + 3081$	0.97	< 0.01				
Note: x is the direction angle; y is the chord angle							

To identify the specific relationship between the stress wave velocity and the space angle with different moisture contents, nonlinear regression analysis was performed to establish the regression model of stress wave propagation velocity, direction angle, chord angle, and moisture content (Table 5).

Table 5. Regression Model of Stress Wave Propagation Velocity in Threedimensional Space

Range of	Regression Model $y = Ax_1^2 + Bx_2^2 + Cx_3 + D$									
Moisture Content	у	X 1	X 2	X 3	А	В	С	D	R ²	Р
MC > 30%	V	β	α	MC	0.048	-0.046	-543	3559	0.98	< 0.01
MC < 30%	V	β	α	MC	0.047	-0.045	-4284	4863	0.97	< 0.01
Note: MC is moisture content; V is stress wave propagation velocity										

Comparing the regression model with the theoretical model, the coefficient A of the regression model was positive and almost unchanged. In addition, whether the moisture content was above or below the FSP, the ratio of v_R to v_l should remain the same in the theoretical model, so the coefficient (A) of the regression model was consistent with the coefficient of direction angle (β) of the theoretical model. The absolute value of coefficient *B* was almost equal, which was consistent with the coefficient of the chord angle (α) in the theoretical model.

On the basis of the theoretical model, the effect of moisture content on the propagation velocity was introduced, and the regression model of the four factors was established. As the determination coefficients (\mathbb{R}^2) were above 0.97 and the significance (P) was less than 0.01, the models had a high fitting degree. Therefore, the propagation velocity of stress waves in larch wood with different moisture contents in three-dimensional space can be estimated with the regression model.

CONCLUSIONS

- 1. The variation of stress wave propagation velocity in different direction angle and chord angle of wood was analyzed, and a theoretical model of the propagation velocity was established in wood three-dimensional space. The stress wave propagation velocity model satisfied the function formula, $v_r + v_r(1 - v_r / v_l)\beta^2$, in different direction angles of the longitudinal section and the function formula, $v_R [1 - (1 - G_{RT} / E_R)\alpha^2]$, in different chord angles of the cross-section. The two formulas were integrated to obtain a simplified velocity model of three-dimensional space: $f(\alpha, \beta) \approx v_R + (1 - v_R / v_l)v_R \cdot \beta^2 - (1 - G_{RT} / E_R)v_R \cdot \alpha^2$.
- 2. Non-destructive stress wave testing was completed for larch wood with different moisture contents. Propagation velocity models of stress waves in different direction angles and chord angles of wood samples with different moisture contents were established. The test results showed that the effects of the change of direction angle and chord angle on the propagation velocity of stress wave were similar with different moisture contents. The propagation velocity gradually decreased as moisture content increased, and the stress wave velocity was more noticeably affected by moisture content when moisture content was below FSP. In addition, the propagation velocity increased as direction angle increased and decreased as chord angle increased.
- 3. On the basis of the theoretical model and the regression models of stress wave velocity, direction angle, chord angle, and moisture content were established. The regression analysis results showed that the models had a high degree of fitting ($R^2 \ge 0.97$, P < 0.01). Therefore, they can be used to estimate the propagation velocity of stress waves in the three-dimensional space of larch wood under different moisture contents.

ACKNOWLEDGMENTS

The authors are grateful for the support of the Natural Science Foundation of Heilongjiang Province of China (Grant No. LC2018012), the 2020 Special Foundation Project of Fundamental Scientific Research Professional Expense for Undergraduate Universities in Heilongjiang Province.

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Article submitted: March 29, 2020; Peer review completed: June 20, 2020; Revised version received and accepted: July 5, 2020; Published: July 10, 2020. DOI: 10.15376/biores.15.3.6680-6695